

On the interaction of granite with Tc (IV) and Tc (VII) in aqueous solution

Trygve E Eriksen, Daquing Cui

Royal Institute of Technology, Department of Nuclear Chemistry, Stockholm, Sweden

October 1991

SVENSK KÄRNBRÄNSLEHANTERING AB SWEDISH NUCLEAR FUEL AND WASTE MANAGEMENT CO BOX 5864 S-102 48 STOCKHOLM TEL 08-665 28 00 TELEX 13108 SKB S TELEFAX 08-661 57 19

ON THE INTERACTION OF GRANITE WITH TC(IV) AND TC(VII) IN AQUEOUS SOLUTION

Trygve E Eriksen, Daquing Cui

Royal Institute of Technology, Department of Nuclear Chemistry, Stockholm, Sweden

October 1991

This report concerns a study which was conducted for SKB. The conclusions and viewpoints presented in the report are those of the author(s) and do not necessarily coincide with those of the client.

Information on SKB technical reports from 1977-1978 (TR 121), 1979 (TR 79-28), 1980 (TR 80-26), 1981 (TR 81-17), 1982 (TR 82-28), 1983 (TR 83-77), 1984 (TR 85-01), 1985 (TR 85-20), 1986 (TR 86-31), 1987 (TR 87-33), 1988 (TR 88-32), 1989 (TR 89-40) and 1990 (TR 90-46) is available through SKB.

ON THE INTERACTION OF GRANITE WITH Tc(IV) AND Tc(VII)

IN AQUEOUS SOLUTION.

Trygve E Eriksen and Daqing Cui

Royal Institute of Technology, Department of Nuclear Chemistry

S-100 44 Stockholm 70

ABSTRACT

The behaviour of technetium in granite-groundwater systems under reducing conditions was investigated. The anion $TcO_4^$ was reduced to Tc(IV) and simultaneously precipitated as $TcO_2 \cdot nH_2O$ on the granite surfaces. The electron sources are assumed to be iron oxides and/or iron containing minerals in the granite.

The technetium concentration in ground water under repository conditions may be predicted assuming $TcO_2 \cdot nH_2O$ as the solid phase and $TcO(OH)_2^O$ and TcO_4^- as the predominant aqueous complexes using a formation constant for $TcO(OH)_2^O$ of log K = -8.16 and a standard reduction potential E^O for the reaction $TcO_4^- + 3e^- + 4H^+ = TcO_2 \cdot nH_2O$ of 0.738 V. The surface related distribution ratio K_a for $TcO(OH)_2^O$ between Stripa granite and ground water is approximately 1 cm based on geometrical surface area. i

TABLE OF CONTENTS

ABSTRACT					
TAB	LE OF CONTENTS	ii			
1.	INTRODUCTION	1			
2.	EXPERIMENTAL	3			
2.1	Materials	3			
2.2	Column experiment	4			
2.3	TcO ₂ (s) experiment	5			
3. EXPERIMENTAL RESULTS					
3.1	Column experiment	6			
3.2	TcO ₂ (s) experiment	8			
4.	DISCUSSION	10			
5.	REFERENCES	14			
	FIGURES	16-37			

1 INTRODUCTION

The long-lived fission product ${}^{99}\text{Tc}$ (t_{1/2} =2.13 \cdot 10⁵ y) is present in large quantities in nuclear wastes and hence its chemical behaviour in the geosphere is of considerable interest.

When radioactive waste in an underground repository is exposed to groundwater radionuclides it can be leached out and become dispersed by diffusion in the backfill material and the connected microstructure of the host rock. The radionuclides may also be transported through the fracture network of the host rock by advective flow. It is imperative that under no circumstances hazardous quantities of radionuclides reach the biosphere. The radionuclide concentration at the source will be determined by the solubility and the migration retarded if the radionuclide is strongly sorbed on the rock. The solubility and sorption of multivalent redox sensitive radionuclides, like ⁹⁹Tc, depend on the redox properties of the groundwater and the surrounding rock, pH and concentration of complexing agents in the ground water. We have in earlier works studied the migration of Tc in granitic drill cores containing natural fissures under oxic and reducing (+260 to -280 mV) conditions (Eriksen 1985, 1988). Based on the retardation of Tc under reducing conditions and the geometric surface area of the fissure walls the surface related distribution coefficient R_a, defined as the ratio between the concentration of sorbed Tc (mol·cm⁻²) and the concentration of Tc in ground water (mol·cm⁻³), was found to be approximately 1 cm.

An important factor in the assessment of of the migration of a radionuclide is the maximum attainable concentration under the given conditions of water chemistry. Under oxic conditions technetium exists as the anionic species TcO_4^- whereas under reducing conditions, expected to exist in a deep bedrock repository for used fuel, it is generally predicted that technetium will be present as the sparingly soluble $Tc(IV)O_2 \cdot 2H_2O$.

Meyer et al (1986, 1987, 1988,1989) have carried out extensive studies on the solubility of precipitated and electrodeposited Tc(IV) oxides in aqueous solution at pH < 9.7 and the dependence of the solubility of $TcO_2 \cdot nH_2O$ in aqueous solution on pH and pCO₂ has recently been studied by Eriksen et al (1991). From the experimental results it is concluded that the solubility in granitic ground water $(2 \cdot 10^{-3} \text{ mol} \cdot dm^{-3} \text{ HCO}_3^{-},$ pH \approx 8.2) is $6.8 \cdot 10^{-9} \text{ mol} \cdot dm^{-3}$ with $TcO(OH)_2^O$ as the predominant aqueous complex.

The purpose of this work is to study the behaviour of the $TcO_4^{-}/TcO_2 \cdot nH_2O$ redox couple in granite-water systems. The study encopasses two laboratory experiments.

In the first experiment we followed the reduction of TcO_4^- in reducing ground water circulating through a column of coarsly crushed granite.

In the second experiment we studied migration of Tc from $TcO_2 \cdot nH_2O$, electrodeposited on a platinum mesh electrode, to crushed granite in moderately reducing water (E_h approx - 90 mV).

2

2 EXPERIMENTAL

2.1 Materials

All reagents, of analytical grade, were used without further purification.

The radionuclides used were 99 Tc, delivered in 0.1 mol·dm⁻³ NH₄OH aqueous solution from Amersham, and 99m Tc recovered as TcO₄⁻ in 0.4 mol·dm⁻³ aqueous KCl solution from a 99 Mo generator (Kjeller).

Radionuclide solutions were prepared by diluting aliquots of the stock solutions with ground water.

Reducing groundwater was prepared by contacting argon purged (AGA 5.7-quality) triple distilled water with granitic rock in a quartz reservoir as described by Wikberg (1987) and Eriksen (1988). The rock used is granitic rock from the Stripa mine taken at a depth of 360m below ground level.

The redox potentials were monitored with a Metrohm Pt electrode and a Yokogawa SR 20/AR 24 (Ag/AgCl) reference electrode connected to a Metrohm 632 pH meter. The electrodes were standarized using saturated quinhydrone buffers at pH 4 and 7. The pH measurements were performed with a Radiometer pHM84 pH meter and a GK 2321c combined glass/reference electrode.

Both experiments were carried out in a controlled atmosphere box flushed with AGA 5.7-quality Ar containing < 0.5 ppm O₂.

2.2 Column experiment

The experimental set up is depicted in Figure 1. The column was filled with 82 cm³ granitic coupons with approximate dimensions 1x1x1 cm and the entire flow system (total volume 201 cm³) flushed with Ar.

Reducing groundwater from the reservoir was thereafter circulated through the column for several days to equilibrate the granite surfaces. The Tc-experiment was initiated by injecting 15 μ l TcO₄⁻ solution ,initially containing 0.335 mol·dm⁻³ ⁹⁹Tc and approximately 10⁻¹¹ mol·dm⁻³ ^{99m}Tc, into the circulating water. The water flow was 0.18 cm³·min⁻¹ and the measured potential varied between -440 and -460 mV during the experiment.

The Tc transport through the column was initially followed by monitoring the activity of the shortlived 99m Tc (t_{1/2} = 6h) with a NaI scintillation detector fitted with a 20x4 mm lead collimator.

The water circulation was stopped after 4 days and samples were drawn from the water phase and analyzed for TcO_4^- and Tc(IV). The water samples were added to equivalent volumes of chloroform containing 0.1 mol·dm⁻³ tetraphenylarsonium chloride. The organic phase removes TcO_4^- quite efficiently leaving the Tc(IV)-species in the aqueous phase. Testing the extraction procedure we found that two consecutive extractions were sufficient to ensure complete removal of TcO_4^- . Following each extraction, samples from the organic and aqueous phase respectively were mixed with Ready Safe Liquid scintillation coctail (Beckman). The samples were analyzed for the pure β -

emitter 99 Tc (E = 0.293 MeV) in a Beckman model 5801 Liquid scintillation system, calibrated with standard solutions containing appropriate and known 99 Tc concentrations. The water was thereafter removed from the column and the granite coupons divided into eight fractions according to height above the TcO₄⁻ injection point. Each fraction was subdivided into two parts containing approximately 10 g granite and desorption of 99 Tc was carried out following two different procedures.

- each sample was quickly rinsed in Ar-purged distilled water before being transferred to 20 cm^3 flasks containing 10 cm^3 aerated water
- the samples were directly transferred to 20 $\rm cm^3$ flasks containing 10 $\rm cm^3$ aerated water.

The desorption was carried out for 104 days. The flasks were at appropriate intervals, following additions of H_2O_2 and HNO_3 , placed in an ultrasonic bath for 30-40 minutes. The Tc concentration in the aqueous phase was determined by liquid scintillation counting of ^{99}Tc .

2.3 TcO2(s) experiment

The experimental arrangement is depicted in Figure 2. Small glass vials with porous walls were filled with crushed and size fractionated granite and placed a large vessel (approximately 2 dm³) together with 130 g small granitic drill cores (2-4 cm diameter). The vessel was sealed and freed from

oxygen by Ar purging for two days and thereafter filled with 1.8 dm³ water, which had been preequilibrated with granitic rock for eight days in the "ground water generator" (Wikberg, 1987; Eriksen, 1988). $TcO_2 \cdot nH_2O$, electrodeposited on a platinum net, was immersed into the water and water samples were drawn at intervals and analyzed for Tc(IV) and TcO_4^- as described above.

At the end of the experiment the different size fractions of crushed granite were quickly rinsed with reducing water from the ground water generator and transferred into small flasks containing 19.2 cm³ Ar purged water from the generator. After two days in the controlled atmosphere box the flasks were taken out of the box ,opened and aerated. At intervals, following additions of H_2O_2 and/or HNO_3 , the flasks were placed in an ultrasonic bath for 30-40 minutes. The total Tc concentration in the aqueous phase was determined by liquid scintillation counting of 99 Tc.

3. EXPERIMENTAL RESULTS

3.1 Column experiment

The dispersion of Tc in the granite column, monitored by measurement of the 99m Tc activity, following the injection of TcO₄⁻ to the circulating reducing water is shown in Figure 3 and the break through of Tc into the water phase, measured 2 mm above the granite column, is shown in Figure 4. The Tc(IV) and Tc(VII) concentrations in the circulating water 3 and 4 days after the TcO₄⁻ addition respectively are given in Table 1.

Table 1.

Concentration of Tc(IV) and TcO_4^- in the circulating water.

Time after TcO_4^- Tc(IV) TcO_4^- injection (days) $mol \cdot dm^{-3}$ $mol \cdot dm^{-3}$ *

0		4.22.10-5
3	1.12.10-8	$3.89 \cdot 10^{-5}$
4	1.17.10-8	3.90·10 ⁻⁵

* assuming complete mixing (15 μ l 0.335 mol·dm⁻³ TcO₄⁻ added to 119 cm³ circulating water).

As seen, whereas the TcO_4^- concentration in the circulating water decreased by $0.32 \cdot 10^{-5} \text{ mol} \cdot dm^{-3}$ only $1.17 \cdot 10^{-8}$ mol·dm⁻³ was retrieved as Tc(IV) in solution. The Tc(IV)concentration is but slightly higher than the solubility of $TcO_2 \cdot nH_2O$ as determined by Eriksen et al (1991). The granite coupons used for desorption/leaching of Tc were sampled at appropriate positions in the granite column (see Figure 5). The release of Tc from rinsed and unrinsed coupons are plotted in Figures 6-8 and 9-10 respectively. In both cases there is a marked increase in the amount of released 99_{Tc} , given as activity (cpm) per gram granite, with increasing height in the upper part of the granite column. Based on the desorption profile in the column and the total weight of the granite we estimate the total amount of Tc retrieved from the granite samples to be $(2.7+/-0.5) \cdot 10^{-7}$

moles, corresponding to a $(2.3 + -0.5) \cdot 10^{-6} \text{ mol} \cdot \text{dm}^{-3}$ decrease in the TcO₄⁻ concentration of the circulating water.

3.2 TcO₂(s) experiment

The redox potential was monitored continuously throughout the various experimental phases. As can be gleaned from section A of Figure 11 constant E_h was obtained in the groundwater generator after approximately one week. Groundwater was thereafter pumped into the vessel containing the crushed granite (section B). The platinum mesh electrode with electrodeposited $TcO_2 \cdot nH_2O$ was lowered into the water at B/C and water samples drawn for $Tc(IV)/TcO_4^-$ analysis after 43, 46, 50 and 51 days respectively. The concentrations and redox potentials on the normal hydrogen electrode scale are given in Table 2.

Applying Nernst equation

 $E = E^{O} + 2.3(RT/nF) \cdot \log(P_{i} \text{ ox } n^{i}/P_{j} \text{ red } n^{j})$ to the reaction

 $TcO_4^- + 3e^- + 4H^+ = TcO_2 \cdot nH_2O$ we can, using $E^O = 0.738 V$ (Meyer et al 1989) calculate the expected equilibrium concentration of TcO_4^- at the experimental pH and redox conditions. As can be seen from Table 2 ,the measured TcO_4^- concentrations are 2-3 times higher than the calculated ones. It should, however, be pointed out that the uncertainty in the measured redox potential is 15-20 mV which may account for the discrepancies between calculated and measured concentrations.

Table 2.

Redox potential, pH, Tc(IV) and TcO_4^- concentrations for samples of the water phase.

Time	рH	_{Eh} (1)	Tc(IV) 10 ⁹	TcO4 ¹⁰⁵	
days		mV	$mol \cdot dm^{-3}$	$mol \cdot dm^{-3}$	
				measured	calc*
43	9.18	-90	4.8+/-1.7	2.1	0.49
46	9.18	-92	4.2+/-1.5	2.24	0.39
50	9.18	-85	5.6+/-0.1	2.40	0.88
51	9.18	-83	4.7+/-0.2	2.51	1.10

(1) rel normal hydrogen electrode, (ref electrode +226 mV)* calculated using the equation:

 $E = 0.738 + 0.0197 \log [TcO_4] - 0.0788 PH$

The Tc concentrations in reducing water due to release of Tc from the crushed granite are plotted versus the size fractions in Figure 12. As can be seen the measured Tc concentrations correspond to the solubility of TcO₂ • nH₂O (Eriksen et al 1991). The slight increase in the Tc concentrations with time is probably caused by slow intrusion of oxygen into the flasks.

The effect of aerating the bottles on the release of Tc from the crushed granite is very small (Figure 13), indicating a slow reaction with oxygen, whereas addition of H_2O_2 results in a marked increase in the Tc release.

Assuming that the Tc, released from the crushed granite, was sorbed as Tc(IV) we have, based on the concentration of Tc(IV) species in the vessel, calculated a formal distribution ratio (R_d) for each size fraction. The distribution ratios are plotted versus the size fractions in Figure 14. There is clearly no consistent correlation between the distribution ratio and the particle size, the increase in R_d with decreasing particle size in the size range 250-2000 μ m is followed by a sudden decrease in R_d for particels smaller than 250 μ m.

4 DISCUSSION

From the column experiment it may be concluded that the oxidation of TcO_4^- in reducing groundwater is very slow. Most, if not all, of the TcO_4^- dissappearing from the circulating water is sorbed or precipitated on the granite. The concentration of Tc(IV) species in the circulating water corresponds to the solubility of $TcO_2^{-}nH_2^{-}O$ clearly indicating surface deposition of the oxide.

In the $TcO_2(s)$ experiment the TcO_4^- concentration in the aqueous phase is, within the experimental uncertainty, in agreement with the concentration calculated for the $TcO_2 \cdot nH_2O/TcO_4^-$ redox couple using the Nernst equation. In an earlier study of sorption on crushed granite (Eriksen and Locklund 1989) we measured the N₂-BET surface area of crushed and intact granites. The experimental results were accommodated by a model of porous particles with accessible outer and inner surfaces. On linear regression analysis of the

10

 R_d /surface area data for ${}^{99}Tc$ in the size range 250-2000 μ m we obtain an intercept with the surface area axis at 0.24 m²·g⁻¹. Corresponding plots of our earlier data on sorption of ${}^{85}Sr$, 134Cs and 152Eu and cationic exchange capacity of crushed granites are shown in Figures 16-21. With the notable exception of ${}^{152}Eu$ sorption the regression lines pass close to or through origo. An intercept with the surface area axis at 0.24·m² g⁻¹ for Stripa granite indicates that only outer surfaces have participated in the process. In the case of 152Eu this was explained as being due to strong sorption resulting in depletion of ${}^{152}Eu$ in the aqueous phase and thereby slow diffusion and redistribution on the inner surfaces.

We have in an earlier report discussed the migration of Tc in natural granitic fissures under reducing conditions (Eriksen et al 1985, 1988). Based on the retardation of Tc relative to water we estimated the geometric surface based distribution ratio R_a for Tc(IV) between granite and ground water to be 1 cm.

Assuming the crushed granite to consist of spherical particles with diameters equal to the arithmetic means of the sieves bracketing the various size fractions we estimate R_a to be approximately 60 cm in the $TcO_2(s)$ experiment, i.e nearly two orders of magnitude higher than the R_d obtained in the migration experiments.

We have hitherto used the term sorption to describe the loss of a radionuclide from an aqueous solution phase to a contiguous solid phase. Sorption may occur by several 11

mechanisms eg precipitation, (formation of a solid phase) and adsorption (Sposito 1986).

The migration experiments were carried out with total Tc concentration at or lower than the solubility limit of $TcO_2 \cdot nH_2O$ whereas a solid $TcO_2 \cdot nH_2O$ phase as well as Tc(IV) and TcO_4^- in solution were present in the $TcO_2(s)$ experiment. It is evident that the chemical system in the latter experiment is more complicated and several sorption processes may be involved.

A plausible explanation to the apparent disagreement between the R_a values obtained in the two experiments would be that the distribution ratio measured in the migration experiment characterises adsorption of the aqueous Tc(IV) species $TcO(OH)_2^{O}$ on the granite whereas both reduction/precipitation of TcO_4^{-} and sorption of $TcO(OH)_2^{O}$ occured in the $TcO_2(s)$ experiment, thereby yielding a higher R_a value.

The transfer of Tc from the $TcO_2 \cdot nH_2O$ electrode to the crushed granite can be accommodated by a process involving dissolution of Tc(IV) from the electrode, oxidation of aqueous Tc(IV) to TcO_4^- and surface mediated reduction/precipitation of TcO_4^- as $TcO_2 \cdot nH_2O$ on the granite surface.

Data from sorption studies of iron containing minerals (Vandergraaf 1984), iron oxyhydoxides (Walton 1986) and a Fourier transform infrared study of technetium-iron oxide reactions (Haines 1987) clearly demonstrate that TcO_4^- is reduced to $TcO_2 \cdot nH_2O$ and precipitated on the mineral surfaces.

Thus the reduction of TcO_4^- and precipitation of $TcO_2 \cdot nH_2O$ on the granite surfaces is most probably caused by small amounts of iron containing minerals or oxides in the granite. A possible cause of the sudden drop in $TcO_2 \cdot nH_2O$ precipitation for particles <250 μ m is Fe-depletion in the smaller size fractions during the crushing and size fractionation process.

5 REFERENCES

Eriksen T E (1985). A laboratory study of radionuclide migration in single natural fissures. Nuclear Technology <u>70</u>, 261-267.

Eriksen T E (1988). Radionuclide transport in a single fissure. A laboratory flow system for transport under reducing conditions. SKB TR 88-28

Eriksen T E and Locklund B (1989). Radionuclide sorption on crushed and intact granitic rock. Surface and volume effects. SKB TR 89-25.

Eriksen T E , Ndadalamba P, Bruno J and Caceci M (1991) The solubility of $TcO_2 \cdot nH_2O$ in neutral to alkaline solutions under constant pCO_2 . (for Migration 91 in Jerez de la Frontera, October 21-25, 1991.)

Harris R I, Owen D G, Vandergraaf T T (1987). Tecnetium-iron oxide reactions under anoxic conditions. A Fourier Transform Infrared, FTIR study. Nuclear J. of Canada 1:1,32-37.

Meyer R E, Arnold W D and Case F I (1986). Valence effects on solubility and sorption. The solubility of Tc(IV) oxides. NUREG/CR 4309 ORNL-6199.

Meyer R E, Arnold W D and Case F I (1987). The solubility of electrodeposited Tc(IV) oxides. NUREG/CR 4865 ORNL 6734.
Meyer R E, Arnold W D, Case F I and O'Kelly G D (1988). Thermodynamic properties of Tc(IV) oxides; solubilities and the electrode potential of the Tc(VII)/Tc(IV) oxide couple. NUREG/CR 5108 ORNL 6480.

Meyer R E, Arnold W D, Case F I and O'Kelly G D (1989). Solubilities of Tc(IV) oxides and the electrode potential of the Tc(VII)/Tc(IV) oxide couple. NUREG/CR 5235 ORNL 6503.

Sposito G (1986).

Distinguishing adsorption from surface precipitation. In "Geochemical processes of mineral surfaces", ACS Symposium Series No 323, 217-228, Davis and Hayes (eds).

Vandergraaf T T, Ticknor K V and George I M (1984). Reactions between technetium in solution and iron containing minerals under oxic and anoxic conditions. ACS Symposium Series No 246. Geochemical Behavior of Disposed Radioactive Waste. Eds Barney G S, Navratil J D and Schultz W W, pp 25-42.

Walton F B, Paquette J, Ross J P M and Lawrence W E (1986). Tc(IV) and Tc(VII) interactions with iron oxyhydroxides. Nuclear and Chemical Waste Management Vol 6, pp 121-126.

Wikberg P (1987): The chemistry of deep groundwaters in crystalline rocks. Thesis, Dept inorg chemistry. Royal Institute of Technology, Stockholm.



Fig. 1 Schematic illustration of granite Column experiment.



Fig. 2. Schematic illustration of $TcO_2(s)$ experiment.



Activity (cpm)

Figure 3.

^{99m}Tc distribution in granite column after TcO⁻ injection into circulating water.



Figure 4.

^{99m}Tc activity in water phase 2mm above the granite column.



Figure 5.

Positions of granite column samples for leaching of adsorbed/precipitated ⁹⁹Tc.





Activity of ⁹⁹Tc released from rinsed granite-column samples.



Figure 7.

Activity of ⁹⁹Tc released from rinsed granite-column samples.

 \star 0.1 cm 3 0.2N HNO added to samples 2,3,6,7,8. 3 Ultrasonic agitation for 30 min on addition.



Figure 8.

Activity of ⁹⁹Tc released from rinsed granite-column samples.

(1) 0.1 ml 0.2M HNO added to 1.4.5 (2) 0.15 ml H_{2}^{O} added³ to all samples.

Ultrasonic agitation for 30 min on addition.



Figure 9.

Activity of ⁹⁹Tc released from granite-column samples (not rinsed).

(1) 0.1ml 0.2M HNO3 added to 2,3,6,7,8.

Ultrasonic agitation for 30 min on addition.



Figure 10.

Activity of ⁹⁹Tc released from granitecolumn samples (not rinsed).

> (1) 0.1 cm³ 0.2M HNO₃ added to 2,3,6,7,8. (2) 0.1 cm³ 0.2M HNO₃ added to 1,4 0.15 cm³ H₂O₂ added to all samples.





E_h time plot for TCO₂(s) experiment
A: ground-water gerator ; B: water in electrode vessel
B/C: immersion of TcO₂-electrode ; D: sampling period



Figure 12.

 ^{99}Tc released into reducing water from crushed Stripa granite. Full line corresponds to solubility of TcO_2(s).

Size fractions (µm): 1 (63-125); 2 (125-250) 3 (250-500); 4 (250-750); 5 (500-750); 6 (1000-2000) 7 (1000-2000)



Figure 13.

Activity of ⁹⁹Tc released from crushed Stripa granite.

0-2d reducing water, 2-3d air saturated water 3-4d 0.6M ,4-11d 1.4M H $\stackrel{\rm H}{_{\rm 2}}{_{\rm 2}}{_{\rm 2}}{_{\rm 2}}$ 11d 100 μ l HNO $_{_{\rm 3}}$

Ultrasonic agitation on air saturation and additions.



Figure 14.

Distribution ratio R plotted vs particle fraction. Calculation based ^d on amount of ⁹⁹Tc released from crushed granite and Tc(IV) solubility (6.8^{-10⁻⁹} mol^{-dm⁻³}).

Particle size (µm): 1 (63-125); 2 (125-250); 3 (250-500) 4 (250-750); 5 (500-750); 6 (750-1000); 7 (1000-2000)



Figure 15.

Activity of 99 Tc released from crushed Stripa granite plotted versus (N) BET surface area.



Figure 16.

 ^{152}Eu sorption on crushed Stripa granite. Surface area measured by N $_2$ sorption.



Figure 17.

Cationic exchange capacity (CEC) of crushed Stripa granite plotted vs (N) BET surface area.


Figure 18.

 $^{134}\mathrm{Cs}$ sorption on crushed Stripa granite. Surface area measured by N $_2$ sorption.



Fig 19.

 ^{85}Sr sorption on crushed Stripa granite. Surface area measured by (N $_2$) sorption.





 ^{85}Sr sorption on crushed granite plotted versus surface area measured by N $_2$ sorption.



Figure 21.

 ^{85}Sr sorption on crushed Pingstaberg granite. Surface area measured by N $_2$ sorption.

List of SKB reports Annual Reports

1977-78 TR 121 **KBS Technical Reports 1 – 120** Summaries Stockholm, May 1979

1979

TR 79-28 **The KBS Annual Report 1979** KBS Technical Reports 79-01 – 79-27 Summaries Stockholm, March 1980

1980 TR 80-26 **The KBS Annual Report 1980** KBS Technical Reports 80-01 – 80-25 Summaries Stockholm, March 1981

1981 TR 81-17 **The KBS Annual Report 1981** KBS Technical Reports 81-01 – 81-16 Summaries Stockholm, April 1982

1982

TR 82-28 The KBS Annual Report 1982 KBS Technical Reports 82-01 – 82-27 Summaries Stockholm, July 1983

1983

TR 83-77 **The KBS Annual Report 1983** KBS Technical Reports 83-01 – 83-76 Summaries Stockholm, June 1984

<u>1984</u>

TR 85-01 Annual Research and Development Report 1984

Including Summaries of Technical Reports Issued during 1984. (Technical Reports 84-01 – 84-19) Stockholm, June 1985

1985

TR 85-20

Annual Research and Development Report 1985

Including Summaries of Technical Reports Issued during 1985. (Technical Reports 85-01 – 85-19) Stockholm, May 1986 1986 TR 86-31 SKB Annual Report 1986 Including Summaries of Technical Reports Issued

during 1986 Stockholm, May 1987

1987 TR 87-33

SKB Annual Report 1987 Including Summaries of Technical Reports Issued during 1987 Stockholm, May 1988

1988 TR 88-32

SKB Annual Report 1988

Including Summaries of Technical Reports Issued during 1988 Stockholm, May 1989

1989

TR 89-40 SKB Annual Report 1989

Including Summaries of Technical Reports Issued during 1989 Stockholm, May 1990

1990 TR 90-46 **SKB Annual Report 1990** Including Summaries of Technical Reports Issued during 1990 Stockholm, May 1991

Technical Reports List of SKB Technical Reports 1991

TR 91-01

January 1991

Description of geological data in SKB's database GEOTAB Version 2

Stefan Sehlstedt, Tomas Stark SGAB, Luleå January 1991

TR 91-02 Description of geophysical data in SKB database GEOTAB Version 2 Stefan Sehlstedt SGAB, Luleå

TR 91-03 **1.** The application of PIE techniques to the study of the corrosion of spent oxide fuel in deep-rock ground waters **2.** Spent fuel degradation

R S Forsyth Studsvik Nuclear January 1991

TR 91-04 Plutonium solubilities

I Puigdomènech¹, J Bruno² ¹Enviromental Services, Studsvik Nuclear, Nyköping, Sweden ²MBT Tecnologia Ambiental, CENT, Cerdanyola, Spain February 1991

TR 91-05 Description of tracer data in the SKB database GEOTAB SGAB, Luleå

April, 1991

TR 91-06 Description of background data in the SKB database GEOTAB Version 2 Ebbe Eriksson, Stefan Sehlstedt SGAB, Luleå

SGAB, Luleå March 1991

TR 91-07 Description of hydrogeological data in the SKB's database GEOTAB Version 2

Margareta Gerlach¹, Bengt Gentzschein² ¹SGAB, Luleå ²SGAB, Uppsala April 1991

TR 91-08 Overview of geologic and geohydrologic conditions at the Finnsjön site and its surroundings

Kaj Ahlbom¹, Šven Tirén² ¹Conterra AB ²Sveriges Geologiska AB January 1991

TR 91-09

Long term sampling and measuring program. Joint report for 1987, 1988 and 1989. Within the project: Fallout studies in the Gideå and Finnsjö areas after the Chernobyl accident in 1986

Thomas Ittner SGAB, Uppsala December 1990

TR 91-10

Sealing of rock joints by induced calcite precipitation. A case study from Bergeforsen hydro power plant

Eva Hakami¹, Anders Ekstav², Ulf Qvarfort² ¹Vattenfall HydroPower AB ²Golder Geosystem AB January 1991

TR 91-11

Impact from the disturbed zone on nuclide migration – a radioactive waste repository study

Akke Bengtsson¹, Bertil Grundfelt¹, Anders Markström¹, Anders Rasmuson² ¹KEMAKTA Konsult AB ²Chalmers Institute of Technology January 1991

TR 91-12

Numerical groundwater flow calculations at the Finnsjön site

Björn Lindbom, Anders Boghammar, Hans Lindberg, Jan Bjelkås KEMAKTA Consultants Co, Stockholm February 1991

TR 91-13 Discrete fracture modelling of the Finnsjön rock mass

Phase 1 feasibility study

J E Geier, C-L Axelsson Golder Geosystem AB, Uppsala March 1991

TR 91-14

Channel widths Kai Palmqvist, Marianne Lindström

BERGAB-Berggeologiska Undersökningar AB February 1991

TR 91-15

Uraninite alteration in an oxidizing environment and its relevance to the disposal of spent nuclear fuel

Robert Finch, Rodney Ewing Department of Geology, University of New Mexico December 1990

TR 91-16 Porosity, sorption and diffusivity data compiled for the SKB 91 study

Fredrik Brandberg, Kristina Skagius Kemakta Consultants Co, Stockholm April 1991

TR 91-17

Seismically deformed sediments in the Lansjärv area, Northern Sweden Robert Lagerbäck May 1991

TR 91-18

Numerical inversion of Laplace transforms using integration and convergence acceleration

Sven-Åke Gustafson Rogaland University, Stavanger, Norway May 1991

TR 91-19

NEAR21 - A near field radionuclide migration code for use with the PROPER package

Sven Norman¹, Nils Kjellbert² ¹Starprog AB ²SKB AB April 1991

TR 91-20 **Äspö Hard Rock Laboratory. Overview of the investigations 1986-1990** P. Starfers, M. Felstein, J. Marketing, M.

R Stanfors, M Erlström, I Markström June 1991

TR 91-21

Äspö Hard Rock Laboratory. Field investigation methodology and instruments used in the pre-investigation phase, 1986-1990 K-E Almén, O Zellman June 1991

<u>TR 91-22</u>

Aspö Hard Rock Laboratory. Evaluation and conceptual modelling based on the pre-investigations 1986-1990

P Wikberg, G Gustafson, I Rhén, R Stanfors June 1991

TR 91-23 Aspö Hard Rock Laboratory. Predictions prior to excavation and the process of their validation

Gunnar Gustafson, Magnus Liedholm, Ingvar Rhén, Roy Stanfors, Peter Wikberg June 1991

TR 91-24

Hydrogeological conditions in the Finnsjön area. Compilation of data and conceptual model

Jan-Erik Andersson, Rune Nordqvist, Göran Nyberg, John Smellie, Sven Tirén February 1991

TR 91-25

The role of the disturbed rock zone in radioactive waste repository safety and performance assessment.

A topical discussion and international overview.

Anders Winberg June 1991

TR 91-26

Testing of parameter averaging techniques for far-field migration calculations using FARF31 with varying velocity.

Akke Bengtsson¹, Anders Boghammar¹, Bertil Grundfelt¹, Anders Rasmuson² ¹KEMAKTA Consultants Co ²Chalmers Institute of Technology

TR 91-27

Verification of HYDRASTAR. A code for stochastic continuum simulation of groundwater flow Sven Norman Starprog AB July 1991

TR 91-28

Radionuclide content in surface and groundwater transformed into breakthrough curves. A Chernobyl fallout study in an forested area in Northern Sweden Thomas Ittner, Erik Gustafsson, Rune Nordqvist SGAB, Uppsala

June 1991

TR 91-29

Soil map, area and volume calculations in Orrmyrberget catchment basin at Gideå, Northern Sweden

Thomas Ittner, P-T Tammela, Erik Gustafsson SGAB, Uppsala June 1991

TR 91-30

A resistance network model for radionuclide transport into the near field surrounding a repository for nuclear waste (SKB, Near Field Model 91)

Lennart Nilsson, Luis Moreno, Ivars Neretnieks, Leonardo Romero

Department of Chemical Engineering, Royal Institute of Technology, Stockholm June 1991

TR 91-31 Near field studies within the SKB 91 project

Hans Widén, Akke Bengtsson, Bertil Grundfelt Kemakta Consultants AB, Stockholm June 1991

TR 91-32

SKB/TVO Ice age scenario

Kaj Ahlbom¹, Timo Äikäs², Lars O. Ericsson³ ¹Conterra AB ²Teollisuuden Voima Oy (TVO) ³Svensk Kärnbränslehantering AB (SKB) June 1991

TR 91-33

Transient nuclide release through the bentonite barrier - SKB 91

Akke Bengtsson, Hans Widén Kemakta Konsult AB May 1991

TR 91-34

SIMFUEL dissolution studies in granitic groundwater

I Casas¹, A Sandino², M S Caceci¹, J Bruno¹, K Ollila³ ¹MBT Tecnologia Ambiental, CENT, Cerdanyola, Spain ²KTH, Dpt. of Inorganic Chemistry, Stockholm, Sweden ³VTT, Tech. Res. Center of Finland, Espoo, Finland September 1991

TR 91-35

Storage of nuclear waste in long boreholes

Håkan Sandstedt¹, Curt Wichmann¹, Roland Pusch², Lennart Börgesson², Bengt Lönnerberg³ ¹Tyréns ²Clay Technology AB ³ABB Atom August 1991

TR 91-36

Tentative outline and siting of a repository for spent nuclear fuel at the Finnsjön site. SKB 91 reference concept

Lars Ageskog, Kjell Sjödin VBB VIAK September 1991

TR 91-37

Creep of OFHC and silver copper at simulated final repository canisterservice conditions

Pertti Auerkari, Heikki Leinonen, Stefan Sandlin VTT, Metals Laboratory, Finland September 1991

TR 91-38

Production methods and costs of oxygen free copper canisters for nuclear waste disposal

Hannu Rajainmäki, Mikko Nieminen, Lenni Laakso Outokumpu Poricopper Oy, Finland June 1991

TR 91-39

The reducibility of sulphuric acid and sulphate in aqueous solution (translated from German) Rolf Grauer

Paul Scherrer Institute, Switzerland July 1990

TR 91-40

Interaction between geosphere and biosphere in lake sediments

Björn Sundblad, Ignasi Puigdomenech, Lena Mathiasson December 1990

TR 91-41

Individual doses from radionuclides released to the Baltic coast

Ulla Bergström, Sture Nordlinder Studsvik AB May 1991

TR 91-42

Sensitivity analysis of the groundwater flow at the Finnsjön study site

Yung-Bing Bao, Roger Thunvik Dept. Land and Water Resources, Royal Institute of Technology, Stockholm, Sweden September 1991

TR 91-43

SKB - PNC

Development of tunnel radar antennas

Lars Falk ABEM, Uppsala, Sweden July 1991

TR 91-44

Fluid and solute transport in a network of channels

Luis Moreno, Ivars Neretnieks Department of Chemical Engineering, Royal Institute of Technology, Stockholm, Sweden September 1991

TR 91-45

The implications of soil acidification on a future HLNW repository. Part I: The effects of increased weathering, erosion and deforestation Josefa Nebot, Jordi Bruno

MBT Tecnologia Ambiental, Cerdanyola, Spain July 1991

TR 91-46

Some mechanisms which may reduce radiolysis

Ivar Neretnieks, Mostapha Faghihi Department of Chemical Engineering, Royal Institute of Technology, Stockholm, Sweden August 1991